## Wrinkling instabilities in soft dielectric plates

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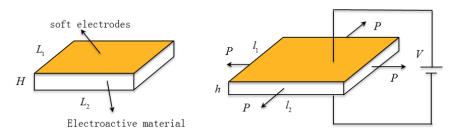
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### Soft Dielectrics

**Soft dielectric materials** are smart materials that deform elastically in the presence of an electric field.



They are modelled by coupling the equations of electrostatics with those of non-linear elasticity.

### Soft Dielectrics

These materials can be used to produce actuators, artificial muscles or wearable electronics.

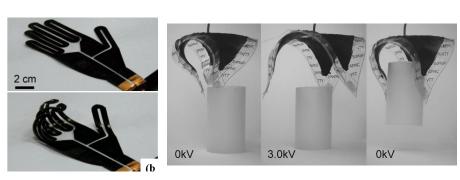


Figure: Applications of dielectric elastomers (Li et al. 2015; Kofod et al. 2007)

**Large deformations** are achieved using the **snap-through** instability.

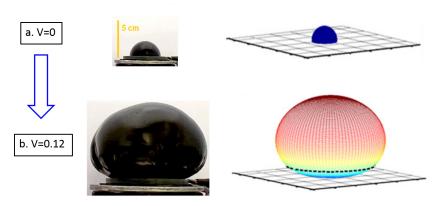
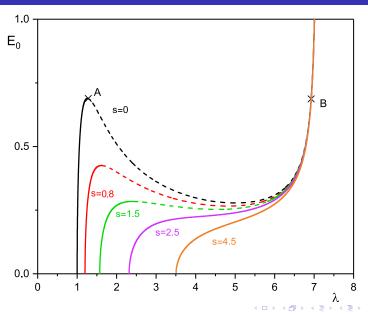
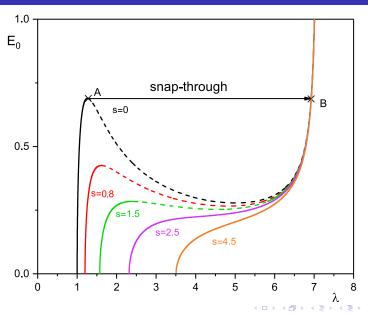
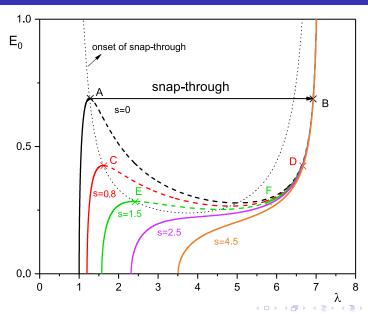


Figure: Experimental evidence of snap-through instability, with area expansion of 1692% (Li et al. 2013)

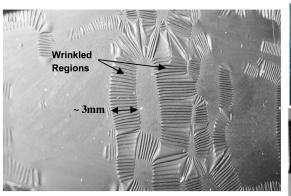






## Wrinkling

Snap-through is difficult to achieve in practice, as the material first breaks down or **wrinkles** form.



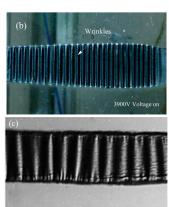
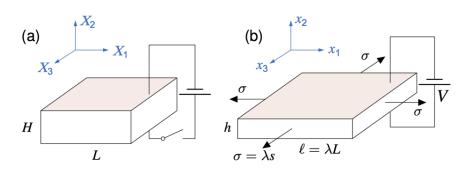


Figure: Experimental evidence of electro-mechanical wrinkling instability (Plante and Dubowsky 2006; Liu et al. 2016; Pelrine et al. 2000)

## Setup of Model

Consider a rectangular plate of soft dielectric material that is **stretched equally** along its lateral directions, principal stretches  $\lambda_1=\lambda_3=\lambda$ ,  $\lambda_2=\lambda^{-2}$ .



We apply a voltage across the thickness direction so that the electric field  $E_L = (0, E_0, 0)$ .

## Setup of Model

We focus on the Gent dielectric, which has energy density

$$\Omega=-rac{J_m}{2}\ln\left(1-rac{(2\lambda^2+\lambda^{-4}-3)}{J_m}
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where  $J_m$  is a stiffening parameter.

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The nominal stress is given by

$$s = \frac{1}{2} \frac{\partial \Omega}{\partial \lambda},$$

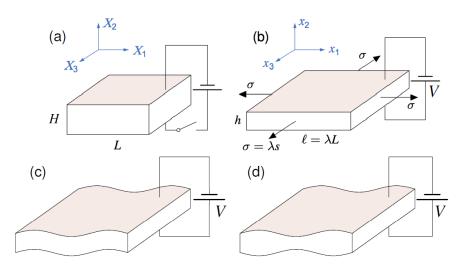
so that the relationship between voltage and stretch is

$$E_0^2 = \frac{\lambda^{-2} - \lambda^{-8}}{1 - (2\lambda^2 + \lambda^{-4} - 3)/J_m} - \lambda^{-3}s.$$

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## Wrinkling Modes

The plate can wrinkle into antisymmetric or symmetric modes.



### Incremental Deformations

We superpose a small **incremental deformation** denoted u onto a finite deformation.



If the incremental motion satisfies the incremental equilibrium equations and boundary conditions, then the material wrinkles.

#### Incremental Deformations

We linearise the equations and solve the problem using the **Stroh formulation**, which reduces the problem to solving the following equation,

$$\eta' = iN\eta,$$

where prime denotes differentiation w.r.t.  $x_2$ , the thickness direction.

This results in an eigen-problem for the eigenvalues and eigenvectors  $\eta$  of the Stroh matrix N.

For **thin-plates**  $(h \rightarrow 0)$ , wrinkling occurs when

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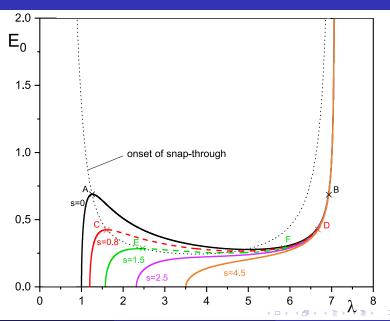
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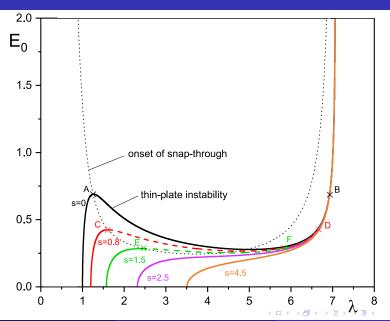
For **thick-plates**  $(h \to \infty)$ , wrinkling occurs when

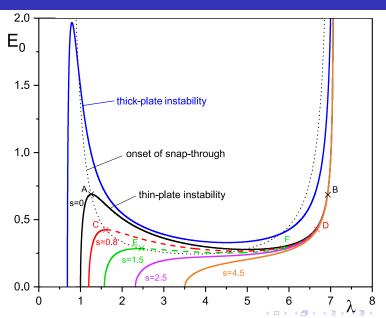
$$\begin{split} 2\lambda(\lambda^9 + \lambda^6 + 3\lambda^3 - 1)W' + 4(\lambda^6 - 1)^2 W'' = \\ \lambda^9(\lambda^3 + 1)E_0^2 \sqrt{1 + 2(\lambda - \lambda^{-2})^2 \frac{W''}{W'}}, \end{split}$$

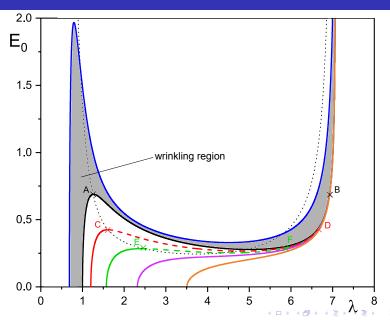
where

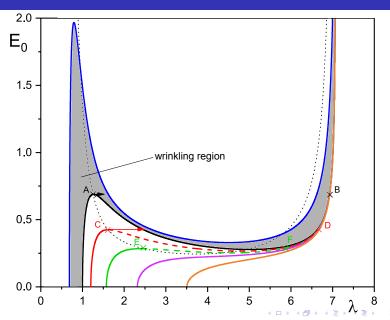
$$W' = \frac{1}{2\left[1 - \left(2\lambda^2 + \lambda^{-4} - 3\right)/J_m\right]}, \qquad W'' = \frac{1}{J_m}W'^2.$$

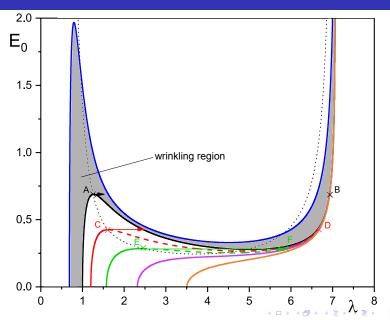




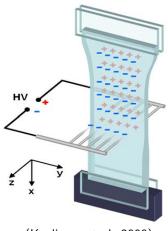








## Charge-controlled actuation

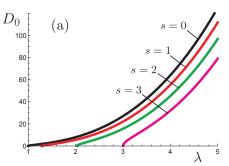


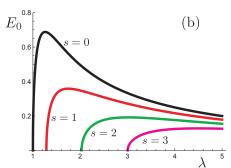
(Keplinger et al. 2009)

- Electric field induced by spraying charges of opposite signs to the lateral faces
- Can wrinkles appear in charge-controlled plates?

## Charge-controlled actuation

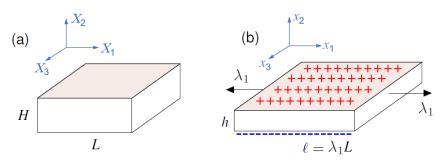
Charge-control is stable with respect to the Hessian criterion.





## Charge-controlled actuation

Consider a rectangular plate of dielectric material, stretched **uniaxially** in the  $x_1$ -direction by  $\lambda_1$ , and charges  $\pm D_0$  applied on its lateral faces.



The charges **induce an electric field**  $E_0$  in the  $x_2$ -direction.

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We focus our attention on **ideal dielectrics**, i.e. materials with energy density

$$\Omega = \frac{1}{2} \left( \lambda_1^2 + \lambda_3^2 + \lambda_1^{-2} \lambda_3^{-2} - 3 \right) - \frac{1}{2} \lambda_1^2 \lambda_3^2 E_0^2,$$

where  $\lambda_3$  is the stretch in the  $x_3$ -direction.

We can then find the following expression for the **charge**  $D_0$ 

$$D_0 = -\frac{\partial \Omega}{\partial E_0}.$$



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$$D_0^2 = \lambda_1^4 \lambda_3^2 - 1.$$

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For **thick-plates**  $(h \to \infty)$ , wrinkling occurs when

$$D_0^4 - \left(\lambda_1^4 \lambda_3^2 + 3\lambda_1^2 \lambda_3 - 2\right) D_0^2 - \left(\lambda_1^6 \lambda_3^3 + \lambda_1^4 \lambda_3^2 + 3\lambda_1^2 \lambda_3 - 1\right) = 0.$$

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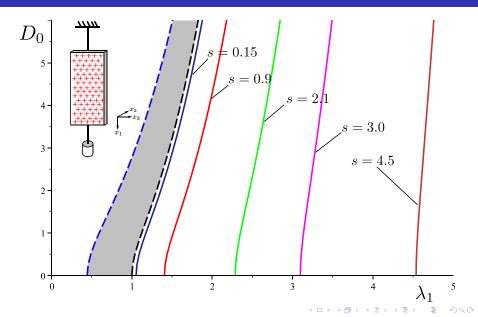
$$D_0^4 - \left(\lambda_1^4 \lambda_3^2 + 3\lambda_1^2 \lambda_3 - 2\right) D_0^2 - \left(\lambda_1^6 \lambda_3^3 + \lambda_1^4 \lambda_3^2 + 3\lambda_1^2 \lambda_3 - 1\right) = 0.$$

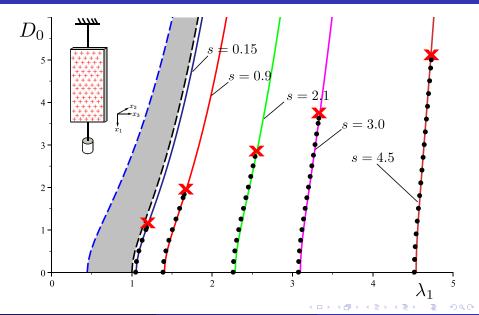
We solve these conditions simultaneously with the loading curve,

$$D_0^2 = \lambda_1^2 \lambda_3^4 - 1,$$

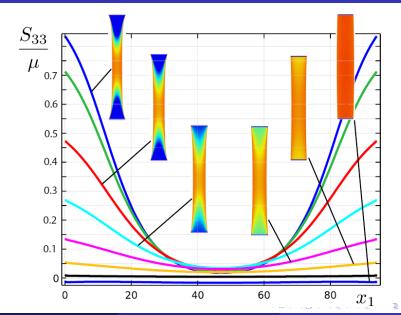
in order to plot  $D_0$  in terms of  $\lambda_1$ .







# Why do the FE Simulations fail?



### Conclusion

- For a real plate, the critical stretch is confined between the thin-plate and thick-plate limits.
- For voltage-controlled actuation, the plates can wrinkle in both contraction and extension.
- Charge-control is **geometrically stable**.
- Overall, charge-control is more stable than voltage-control.

- Y. Su, H. Conroy Broderick, W. Chen, M. Destrade, JMPS, 2018
- H. Conroy Broderick, M. Righi, M. Destrade, R.W. Ogden, preprint 2019